

[of a Minkowski space  $E$ ] with unit bivector  $E = e \wedge e_*$ ; and

associating a plurality of general homogeneous operators with each data construct to generate a model of the object.

3. The method of claim 1 further comprising:

measuring a scalar distance  $d_{ab}$  between two component points  $\mathbf{a}$  and  $\mathbf{b}$  encoded as [general] homogeneous points  $a$  and  $b$  by  $d_{ab}^2 = (a - b)^2 = -2a \cdot b$ .

4. The method of claim 1 wherein a line through component points  $\mathbf{a}$  and  $\mathbf{b}$  encoded as [general] homogeneous points  $a$  and  $b$  is modeled by  $e \wedge a \wedge b$ , and a length  $l_{ab}$  of a line segment connecting component points  $\mathbf{a}$  and  $\mathbf{b}$  is generated by:

$$(l_{ab})^2 = (e \wedge a \wedge b)^2 = (a - b)^2.$$

5. The method of claim 1 wherein a plane through component points  $\mathbf{a}$ ,  $\mathbf{b}$ , and  $\mathbf{c}$  encoded as [general] homogeneous points  $a$ ,  $b$ , and  $c$  is modeled by  $e \wedge a \wedge b \wedge c$ , and an area  $A_{abc}$  [defined by component points  $\mathbf{a}$ ,  $\mathbf{b}$ , and  $\mathbf{c}$ ] is generated by  $(A_{abc})^2 = \frac{1}{4}(e \wedge a \wedge b \wedge c)^2$ .

6. The method of claim 1 wherein a sphere  $s$  with radius  $r$  centered at a component point  $\mathbf{c}$  encoded as a [general homogenous radius  $r$  and center] homogeneous point  $c$  is [generated by] encoded as a vector  $s = c + \frac{1}{2}r^2 e$ .

7. The method of claim 1 wherein a sphere  $s$  determined by four component points  $\mathbf{a}$ ,  $\mathbf{b}$ ,  $\mathbf{c}$ ,  $\mathbf{d}$  encoded as [general] homogeneous points  $a, b, c, d$  is generated by [ $s = IE(a \wedge b \wedge c \wedge d)$ , where  $I$  is a largest k-blade]  $s = (a \wedge b \wedge c)(a \wedge b \wedge c \wedge e)^{-1}$ .

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8. The method of claim [7 wherein one of the general homogeneous] 1 wherein a plane through component points  $a, b$ , and  $c[d]$  encoded as homogeneous points  $a, b$ , and  $c$  is [equal to the point  $e$  so that  $s$  defines a plane through the point  $e$ ] encoded as a vector  $p = I(a \wedge b \wedge c \wedge e) |a \wedge b \wedge c \wedge e|^{-1}$ , where  $I$  is a unit pseudoscalar.

9. The method of claim [5] 8 wherein a distance[s] between a component homogeneous point  $a$  and a component plane  $p$  is generated by an inner product[s]  $a \cdot p$  of an encoded point  $a$  and an encoded plane  $p$ .

10. The method of claim 6 wherein a distance[s] between a component homogeneous point  $a$  and a component sphere  $s$  is [an] generated by an inner product  $a \cdot s$  of an encoded point  $a$  and the encoded sphere  $p$ .

11. The method of claim 6 wherein a distance between two component spheres  $[s_1$  and  $s_2$  encoded as spheres]  $s_1 = c_1 + \frac{1}{2}r_1^2 e$  and  $s_2 = c_2 + \frac{1}{2}r_2^2 e$  is generated by  $\{[s_1 \cdot s_2 = c_1 \cdot c_2 + \frac{1}{2}(r_1^2 + r_2^2) = -\frac{1}{2}[(c_1 - c_2)^2 - (r_1^2 + r_2^2)]\} s_1 \cdot s_2 = c_1 \cdot c_2 + \frac{1}{2}(r_1^2 + r_2^2) \equiv \frac{1}{2}[(r_1^2 + r_2^2) - (c_1 - c_2)^2]$ .

12. The method of claim 1 wherein the object is a rigid body, and a motion of the rigid body is determined by a time dependent displacement verson  $D = D(t)$  satisfying a differential equation  $\dot{D} = \frac{1}{2}VD$ , with “screw velocity”  $V$  given by  $V = -I\omega + e\mathbf{v}$ , where  $\omega$  is a velocity and  $\mathbf{v}$  is a rotational translational velocity of the rigid body.

13. The method of claim 12 wherein *dynamics* of the rigid body are determined by a differential equation  $\dot{P} = W$ , where  $P = -I\mathbf{L} + e_*\mathbf{p}$ , and  $W = -I\mathbf{T} + e_*\mathbf{F}$ , where  $\mathbf{L}$

is an angular momentum and  $\mathbf{p}$  is a translational momentum of the rigid body, while  $\mathbf{T}$  is [the] a net torque and  $\mathbf{F}$  is a net force on the rigid body.

*AN Contd*

14. The method[s] of claim 12 wherein the [rigid body includes] object is composed of  $n$  linked rigid components, and a motion of the [rigid body] object is modeled by  $n$  time dependent displacement versors  $D_1, D_2, \dots, D_n$ , [and] with a motion of a  $k^{\text{th}}$  linked rigid component [is] determined by a versor product  $D_1 D_2 \dots D_k$ .
15. The method of claim 1 wherein the object[s] is a robot composed of a plurality of [links] rigid bodies connected at joints.

## Amended Claims

1. A method for modeling an object composed of one or more components, comprising:
  - inputting data for each component of the object, the data including coordinates expressed in Euclidean space for a plurality of points  $\mathbf{x}$  of each component;
  - encoding each point  $\mathbf{x}$  as a null vector  $x$  in a homogeneous space by  $x = (\mathbf{x} + \frac{1}{2}\mathbf{x}^2 e + e_*)E = \mathbf{x}E - \frac{1}{2}\mathbf{x}^2 e + e_*$ , where  $e$  and  $e_*$  are null vectors with unit bivector  $E = e \wedge e$ ; and
  - associating a plurality of general homogeneous operators with each data construct to generate a model of the object.

3. The method of claim 1 further comprising:

measuring a scalar distance  $\mathbf{d}_{ab}$  between two component points  $\mathbf{a}$  and  $\mathbf{b}$

encoded as homogeneous points  $a$  and  $b$  by  $\mathbf{d}_{ab}^2 = (a - b)^2 = -2a \bullet b$ .

4. The method of claim 1 wherein a line through component points  $\mathbf{a}$  and  $\mathbf{b}$  encoded as homogeneous points  $a$  and  $b$  is modeled by  $e \wedge a \wedge b$ , and a length  $\mathbf{l}_{ab}$  of a line segment connecting component points  $\mathbf{a}$  and  $\mathbf{b}$  is generated by:

$$(\mathbf{l}_{ab})^2 = (e \wedge a \wedge b)^2 = (a - b)^2.$$

5. The method of claim 1 wherein a plane through component points  $\mathbf{a}$ ,  $\mathbf{b}$ , and  $\mathbf{c}$  encoded as homogeneous points  $a$ ,  $b$ , and  $c$  is modeled by

$e \wedge a \wedge b \wedge c$ , and an area  $A_{abc}$  is generated by  $(A_{abc})^2 = \frac{1}{4}(e \wedge a \wedge b \wedge c)^2$ .

6. The method of claim 1 wherein a sphere  $\mathbf{s}$  with radius  $\mathbf{r}$  centered at a component point  $\mathbf{c}$  encoded as a homogeneous point  $c$  is encoded as a vector  $\mathbf{s} = c + \frac{1}{2}r^2e$ .

7. The method of claim 1 wherein a sphere  $\mathbf{s}$  determined by four component points  $\mathbf{a}$ ,  $\mathbf{b}$ ,  $\mathbf{c}$ ,  $\mathbf{d}$  encoded as homogeneous points  $a, b, c, d$  is generated by  $s = (a \wedge b \wedge c)(a \wedge b \wedge c \wedge e)^{-1}$ .

8. The method of claim 1 wherein a plane through component points  $a, b$ , and  $c$  encoded as homogeneous points  $a$ ,  $b$ , and  $c$  is encoded as a vector  $p = I(a \wedge b \wedge c \wedge e)|a \wedge b \wedge c \wedge e|^{-1}$ , where  $I$  is a unit pseudoscalar.

9. The method of claim 8 wherein a distance between a component homogeneous point  $\mathbf{a}$  and a component plane  $\mathbf{p}$  is generated by an inner product  $a \bullet p$ .

10. The method of claim 6 wherein a distance between a component homogeneous point  $\mathbf{a}$  and a component sphere  $\mathbf{s}$  is generated by an inner product  $\mathbf{a} \bullet \mathbf{s}$ .
11. The method of claim 6 wherein a distance between two component spheres  $s_1 = c_1 + \frac{1}{2}r_1^2 e$  and  $s_2 = c_2 + \frac{1}{2}r_2^2 e$  is generated by  $s_1 \bullet s_2 = c_1 \bullet c_2 + \frac{1}{2}(r_1^2 + r_2^2) = \frac{1}{2}[(r_1^2 + r_2^2) - (c_1 - c_2)^2]$ .
12. The method of claim 1 wherein the object is a rigid body, and a motion of the rigid body is determined by a time dependent displacement verson  $D=D(t)$  satisfying a differential equation  $\dot{D} = \frac{1}{2}VD$ , with “screw velocity”  $V$  given by  $V = -I\omega + e\mathbf{v}$ , where  $\omega$  is a velocity and  $\mathbf{v}$  is a rotational translational velocity of the rigid body.
13. The method of claim 12 wherein *dynamics* of the rigid body are determined by a differential equation  $\dot{P} = W$ , where  $P = -I\mathbf{L} + e_*\mathbf{p}$ , and  $W = -I\mathbf{T} + e_*\mathbf{F}$ , where  $\mathbf{L}$  is an angular momentum and  $\mathbf{p}$  is a translational momentum of the rigid body, while  $\mathbf{T}$  is a net torque and  $\mathbf{F}$  is a net force on the rigid body.
14. The method of claim 12 wherein the object is composed of  $n$  linked rigid components, and a motion of the object is modeled by  $n$  time dependent displacement versors  $D_1, D_2, \dots, D_n$ , with a motion of a  $k^{\text{th}}$  linked rigid component determined by a versor product  $D_1 D_2 \dots D_k$ .
15. The method of claim 1 wherein the object is a robot composed of a plurality of rigid bodies connected at joints.